Attorney Docket No: NAVI-009/02US

the specification of which:

**PATENT** 

#### **DECLARATION**

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

#### METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES

7					
then there med the		ereto.			
		[] was filed on	, and identified as Attorney Docket No. NAVI-009/02US.		
i.		[] was filed on	, as Application Serial No.		
	and				
		[] the amendment(s) of which were filed on .			
-	I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above.				

I acknowledge the duty to disclose information which is material to the patentability of this application in accordance with Title 37, Code of Federal Regulations, Section 1.56.

I hereby claim foreign priority benefits under title 35, United States Code, Section 119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

Prior Foreign Application(s) (Country) (Number) (Day/Month/Year Filed)	Priority Claimed (Yes/No)
	Yes
,,	Yes

I hereby claim the benefit under Title 35, United States Code, § 119(e) of any United States provisional application(s) listed below.

60/100,290	September 14, 1998
(Application Number)	(Filing Date)
60/100,224	September 14, 1998
(Application Number)	(Filing Date)
60/109,232	November 18, 1998
(Application Number)	(Filing Date)
60/109,234	November 18, 1998
(Application Number)	(Filing Date)

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, Section 112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, Section 1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application:

Appl. Ser. No.

Filing Date

Status (Pat'd./Pend./Aband.)

I direct that correspondence concerning this application be directed to

COOLEY GODWARD LLP
Attention: Patent Group
Five Palo Alto Square
3000 El Camino Real
Palo Alto, California 94306-2155
Telephone (650) 843-5000.
Facsimile (650) 857-0663

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Full name of sole or First inventor: Grass, George M.					
Inventor's signature	DateDate				
Residence:	Tahoe City, California				
Citizen of:	United States of America				
Post Office Address:	1506 Juniper Mountain Road, P.O. Box 1242 Tahoe City, California 96145				
Full name of sole or Second inver	ntor: Leesman, Glen D.				
Inventor's signature	Date 05/10/89				
Residence:	Hamilton, Montana				
Citizen of:	United States of America				
Post Office Address:	186 Nighthawk Lane Hamilton, Montana 59840-9307				
Full name of sole or Third invent	Full name of sole or Third inventor: Nortis, Daniel A.				
Inventor's signature	Date 5/7/99				
Residence:	San Diego, California				
Citizen of:	United States of America				
Post Office Address:	3145 Cowley Way, #130 San Diego, California 92117				
Full name of sole or Fourth inven	ator: Sinko, Patrick J.				
Inventor's signature	() L Date 5/10/99				
Residence:	Lebanon, New Jersey				
Citizen of:	United States of America				
Post Office Address:	2 Country Place Lebanon, New Jersey 08833				

Full name of sole or Fifth invent	Wehrli, John E.		
Inventor's signature	DateDate		
Residence:	Mountain View, California		
Citizen of:	United States of America		
Post Office Address:	1879 Springer Unit B		

# CONFIDENTIAL

Attorney Docket No: NAVI-009/02US

**PATENT** 

Express Mail Label Number:

EM 570 539 405 US

Date of Deposit:

May 26, 1999

I hereby certify that this paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, DC 20231.

Date

26 May 99

By:

VLADIMIR SKLIBA

#### IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re application of George M. Grass, et al.

Serial No.:

Not yet assigned

Examiner:

Not yet assigned

Filed:

Herewith

Art Unit:

Not yet assigned

For:

METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES

Assistant Commissioner for Patents BOX PATENT APPLICATION Washington, D.C. 20231

# POWER OF ATTORNEY BY ASSIGNEE AND EXCLUSION OF INVENTORS UNDER 37 CFR 1.36 AND 3.71

Sir:

The undersigned assignee of the entire interest in the application for Letters Patent identified above hereby revokes all prior appointments of attorneys and appoints

Nina M. Ashton	37,273	Marcella Lillis	36,583
Alexandra J. Baran	39,101	Tom M. Moran	26,314
James A. Bradburne	38,389	Richard L. Neeley	30,092
Aaron S. Brodsky	39,920	Craig P. Opperman	37,078
Shelley P. Eberle	31,411	Marya A. Postner	42,085
Richard M. Goldman	25,585	Gurjeev K. Sachdeva	37,434
Willis E. Higgins	23,025	William E. Winters	42,232
Peter R. Leal	24,226	Kevin J. Zimmer	36,977

all of the firm of Cooley Godward LLP, to prosecute this application and to transact all business in the United States Patent and Trademark Office connected therewith. This appointment shall be to the exclusion of the above-identified inventor(s) and any attorney(s) appointed by such inventor(s), in accordance with the provisions of 37 C.F.R. 1.36 and 3.71.

Assignee's rights are evidenced by an assignment

- [X] a copy of which is enclosed herewith.
- [] previously recorded on at reel, frame(s).

Please direct all telephone calls and correspondence to:

Cooley Godward LLP Attention: Patent Group Five Palo Alto Square 3000 El Camino Real Palo Alto, CA 94306-2155 Telephone: 650-843-5000

Facsimile: 650-857-0663

Assignee: Navidyte, Inc.  Signature:
Signature:
Name: John K. Wehrli, Esq.
Title: Senior Director, Legal Affairs/ Corporate Secretary
Address: 9880 Campus Point Drive, San Diego, California 92121

Date: May 14, 1999

# CONFIDENTIAL

**PATENT** 

Express Mail Label Number:

EM 570 539 405 US

Date of Deposit:

May 26, 1999

I hereby certify that this paper or fee is being deposited with the United States Postal Service "Express Mail Post Office to Addressee" service under 37 CFR 1.10 on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, DC 20231.

Date:

26 May 99

Bv

VLADIMIR SKLIBA

# IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re application of George M. Grass, et al.

Serial No.:

Not yet assigned

Examiner:

Not yet assigned

Filed:

May 26, 1999

Art Unit:

Not yet assigned

For:

METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES.

Assistant Commissioner for Patents Washington, D.C. 20231

# STATEMENT UNDER 37 CFR 3.73(b) ESTABLISHING RIGHT OF ASSIGNEE TO TAKE ACTION

1. The assignee(s) of the entire right, title and interest hereby seek(s) to take action in the PTO in this matter.

#### **IDENTIFICATION OF ASSIGNEE**

Name of Assignee:	Navicyte, Incorporated	
Type of Assignee:	Corporation	

# PERSON AUTHORIZED TO SIGN

Name	e of Pers	son Authorized to Sign:Jame	es A. Bra	adburne, Ph.D.
Title of Person Authorized to Sign: Agent of Record				
[X]		person signing below, state that I am f of the assignee.	n empow	ered to sign this statement on
		BASIS OF ASSIGNEE	'S INTE	REST
		y the assignee is established as follow t assignee is shown below:	ws. A ch	nain of title from the inventor(s)
	1.	From: George M. Grass, C Patrick J. Sinko and John E. Wehr		Leesman, Daniel A. Norris,
		To: Navicyte, Incorpora	ıted	
		Recordation Date: 12/22/98 Re	el: <u>967</u>	73 Frame: <u>0774-0777</u>
[]	Copie	es of the documents in the chain of ti	tle are att	tached.
Attn:	Patent Palo Ali	ward LLP Group to Square ino Real		Respectfully submitted, COOLEY GODWARD LLP

#### PATENT APPLICATION

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re the Application of:

GRASS et al.

Art Unit: 1631

Application No.: 09/320,069

Examiner: M. Moran

Filed: May 26, 1999

Attorney Dkt. No.: 109904-00027

For: METHOD FOR SCREENING AND PRODUCING COMPOUND LIBRARIES

# REVOCATION OF POWER OF ATTORNEY AND NEW APPOINTMENT

**Assistant Commissioner for Patents** Washington, D.C. 20231

November 5, 2001

Sir:

Dr. Christian Kilger, the undersigned, certifies that Lion Bioscience AG is the assignee of the entire right, title and interest in U.S. Patent Application Serial No. 09/320,069, filed May 26, 1999, by virtue of an assignment from NaviCyte, Inc., a copy of which is attached hereto. The assignment to NaviCyte was recorded in the Patent and Trademark Office at Reel 9673, Frame 0774-0777 on December 22, 1998.

Further, Lion Bioscience AG, as assignee of the entire interest in and to the above-identified United States patent application hereby revokes all powers of attorney previously given and appoints Arent Fox Kintner Plotkin & Kahn, 1050 Connecticut Avenue, Suite 600, Washington, DC, 20036-5339, a firm composed of:

Charles M. Marmelstein, Reg. No. 25,895; Robert B. Murray, Reg. No. 22,980; George E. Oram, Jr., Reg. No. 27,931; Douglas H. Goldhush, Reg. No. 33,125; Richard J. Berman, Reg. No. 39,107; Murat Ozgu, Reg. No. 44,275; Robert K. Carpenter, Reg. No. 34,794; Gregory B. Kang, Reg. No. 45,273; Rustan Hill, Reg. No. 37,351; Kevin F. Turner, Reg. No. 43,437; Rhonda C. Barton, Reg. No. P47,271 and Hans J. Crosby, Reg. No. 44,634, Brian A. Tollefson, Reg. No. 46,338, Lynn D. Anderson, Reg. No. 46,412, David D. Dzara, Reg. No. 47,543; Laurence J. Edson, Reg. No. 44,666; Michael A. Steinberg, Reg. No. 43,160; and Lynn A. Bristol, Reg. No. 48,898.

as principal attorneys to prosecute said application and to transact all business in the Patent and Trademark Office connected therewith.

The undersigned has reviewed all of the appropriate documents and, to the best of the undersigned's knowledge and belief, title is in the assignee identified above.

The undersigned (whose title is supplied below) is empowered to sign this paper on behalf of the assignee.

By the provisions of 28 U.S.C. §1746, I hereby declare under penalty of perjury under the laws of the United States of America that the foregoing is true and correct.

Executed on: November 5, 2001

(date)

Name:

Dr. Christian Kilger

Title:

Director of IP and Licensing

Signature

TECH/48796.1

# ATTACHED SHEET

U.S. Patent 5,183,760

U.S. Patent 5,591,636

U.S. Serial Number 09/320,069

U.S. Serial Number 09/320,270

U.S. Serial Number 09/320,545

U.S. Serial Number 60/224,106

U.S. Patent 5,599,688

U.S. Patent 6,146,883

U.S. Serial Number 09/320,372

U.S. Serial Number 09/320,371

U.S. Serial Number 09/320,544

# <u> ASSIGNMENT</u>

WHEREAS, NaviCyte, Inc. (hereinafter ASSIGNOR) a company having its principal office and place of business at Sparks, Nevada, USA owns the inventions, and the patents and patent applications in various countries directed thereto, as set forth on the 2 page attachment hereto.

AND, WHEREAS, LION Bioscience AG (hereinafter ASSIGNEE), a company having its principal office and place of business at Heidelberg, Germany, is desirous of acquiring all interest therein.

NOW, THEREFORE, in consideration of One Dollar (\$1.00) and other good and valuable consideration, the receipt and sufficiency of which are hereby acknowledged, the above said ASSIGNOR by these presents does sell, assign and transfer unto the said ASSIGNEE, its successors, assigns and legal representatives, the full and exclusive right, title and interest in and to the said inventions in the United States and other countries including the ful and extensive right, title and interest world-wide in and to the patents and patent applications on the attachment hereto.

NaviCyte, Inc.

Title:

Date:

Mitnoce:

6/6/01

# **APPENDICIES**

# Appendix 1: Abbreviation Key for Mass-Volume Model

Abbreviation			
Kf sd = associated rate constant for stomach and duodenum			
Ka dj = associated rate constant for duodenum and jejunum			
Ka ji = associated rate constant for jejunum and ileum			
Ka ie = associated rate constant for ileum and colon			
Ka co = associated rate constant for colon and excretion			
SD trans = transfer rate between stomach and duodenum			
DJ trans = transfer rate between duodenum and jejunum			
JL trans = transfer rate between jejunum and ileum			
IC trans = transfer rate between ileum and colon			
Waste = transfer rate between colon and excretion			
pH s = pH stomach			
pH s2 = pH duodenum			
pH s3 = pH jejunum			
pH s4 = pH ileum			
pH s5 = pH colon			
sol profile = solubility profile for stomach			

sol profile 2 = solubility profile for duodenum		
sol profile 3 = solubility profile for jejunum		
sol profile 4 = solubility profile for ileum		
sol profile 5 = solubility profile for colon		
stom ka = associated rate constant for stomach compartments 1 and 2		
duo ka = associated rate constant for duodenum compartments 1 and 2		
Jej ka = associated rate constant for jejunum compartments 1 and 2		
Il ka = associated rate constant for ileum compartments 1 and 2		
Colon ka = associated rate constant for colon compartments 1 and 2		
SA stom = surface area of stomach		
SA duo = surface area of duodenum		
SA jej = surface area of jejunum		
SA il = surface area of ileum		
SA colon = surface area of colon		
Perm stom = permeability of stomach		
Perm duo = permeability of duodenum		
Perm jej = permeability of jejunum		
Perm il = permeability of ileum		
Perm colon = permeability of colon		

Ka sd = associated rate construct for stomach fluid absorption

Ka du = associated rate construct for duodeunm fluid absorption

Ka je = associated rate construct for jejunm fluid absorption

Ka il = associated rate construct for ileunm fluid absorption

Ka co = associated rate construct for colon fluid absorption

Note: other abbreviations adhere to above descriptors and are self explanatory

# Appendix 2: Equations, Parameters and Values For Mass-Volume Model

```
amt_plasma(t) = amt_plasma(t - dt) + (trans_21 + ka - elimination - trans_12) * dt
     INIT amt plasma = 0
     INFLOWS:
     trans_21 = k21*comp_2
     ka = tot_abs_rate
     OUTFLOWS:
     elimination = amt plasma*k elim
     trans_12 = k12*amt plasma
     blood_side_col(t) = \overline{b}lood_side_col(t - dt) + (colon_ka_5) * dt
     INIT blood side col = 0
INFLOWS:
    colon_ka_5 = IF Vol_colon*sol_profile_5 >=Colon THEN Colon*SA_colon*perm_colon*3600
    ELSE Vol_colon*sol_profile_5*SA_colon*perm_colon*3600
Ф
    blood\_side\_dou(t) = blood\_side\_dou(t - dt) + (duo ka) * dt
₫
ū
    INIT blood side dou = 0
Ш
    INFLOWS:
Ш
    duo ka
=
                         IF
                                 Vol duod*sol profile 2
                                                             >=
                                                                      duodenum
                                                                                      THEN
    duodenum*SA_duo*perm_duo*3600 ELSE Vol_duod*sol_profile_2*SA_duo*perm_duo*3600
ᆣ
blood_side_il(t) = blood_side_il(t - dt) + (Il ka) * dt
N
    INIT blood side il = 0
H
    INFLOWS:
    Il_ka = IF Vol_ileum*sol_profile_4 >=Ileum THEN Ileum*SA_Il*perm_Il*3600
                                                                                      ELSE
    Vol_ileum*sol_profile_4*SA_II*perm_II*3600
    blood_side_jej(t) = blood_side_jej(t - dt) + (Jej ka) * dt
    INIT blood side jej = 0
    INFLOWS:
    Jej_ka = IF Vol_jej*sol_profile_3 >=Jejunum THEN Jejunum*SA_jej*perm_jej *3600 ELSE
    Vol_jej*sol_profile_3*SA_jej*perm_jej*3600
    blood\_side\_sto(t) = blood\_side\_sto(t - dt) + (stom\_ka) * dt
    INIT blood side sto = 0
    INFLOWS:
    stom_ka = IF Vol_stom*sol_profile >= Stomach THEN Stomach*SA_stom*perm_stom*3600
    ELSE Vol stom*sol profile*SA stom*perm stom*3600
    Colon(t) = Colon(t - dt) + (IC trans - Waste - colon ka 5) * dt
    INIT Colon = 0
```

```
INFLOWS:
    IC trans = ka ic*Ileum
    OUTFLOWS:
    Waste = ka col*Colon
    colon_ka_5 = IF Vol_colon*sol_profile_5 >=Colon THEN Colon*SA_colon*perm_colon*3600
    ELSE Vol_colon*sol_profile_5*SA colon*perm colon*3600
    comp 2(t) = comp \ 2(t - dt) + (trans \ 12 - trans \ 21) * dt
    INIT comp 2 = 0
    INFLOWS:
    trans 12 = k12*amt_plasma
    OUTFLOWS:
    trans_21 = k21*comp_2
    duodenum(t) = duodenum(t - dt) + (SD trans - duo ka - DJ trans) * dt
  INIT duodenum = 0
₽
INFLOWS:
SD_trans = if Stomach > 0 then kf_sd*Stomach else 0
I
☐ OUTFLOWS:
duo ka
                       IF
                                Vol duod*sol profile 2
                                                                    duodenum
                                                                                    THEN
duodenum*SA_duo*perm_duo*3600 ELSE Vol_duod*sol_profile_2*SA_duo*perm_duo*3600
    DJ_trans = ka dj*duodenum
   excretion(t) = excretion(t - dt) + (vol cw) * dt
   INIT excretion = 0
ΠJ
   INFLOWS:
   vol cw = Vol colon*ka col
   excretion_2(t) = excretion_2(t - dt) + (Waste) * dt
   INIT excretion 2 = 0
   INFLOWS:
   Waste = ka col*Colon
   Ileum(t) = Ileum(t - dt) + (JL_trans - IC_trans - Il_ka) * dt
   INIT Ileum = 0
   INFLOWS:
   JL_trans = ka ji*Jejunum
   OUTFLOWS:
   IC trans = ka ic*Ileum
   Il_ka = IF Vol_ileum*sol_profile_4 >=Ileum THEN Ileum*SA_Il*perm Il*3600
                                                                                    ELSE
   Vol_ileum*sol profile 4*SA Il*perm Il*3600
   Jejunum(t) = Jejunum(t - dt) + (DJ_trans - JL_trans - Jej ka) * dt
```

```
INIT Jejunum = 0
     INFLOWS:
     DJ_trans = ka_dj*duodenum
     OUTFLOWS:
     JL_trans = ka ji*Jejunum
    Jej_ka = IF Vol_jej*sol_profile_3 >=Jejunum THEN Jejunum*SA_jej*perm_jej *3600 ELSE
    Vol_jej*sol_profile_3*SA_jej*perm_jej*3600
    serosal\_col(t) = serosal\_col(t - dt) + (Adsorp\_col - col\_secretion) * dt
    INIT serosal col = 0
    INFLOWS:
    Adsorp\_col = PULSE(1.67,0,.1) + 0*Vol colon*ka co
    OUTFLOWS:
    col_secretion = 0
    serosal\_dou(t) = serosal\_dou(t - dt) + (Adsorp\_Duo - duo\_secretion) * dt
INIT serosal dou = 0
    INFLOWS:
U
    Adsorp_Duo = PULSE(10.82,0,.1) + 0*Vol_duod*ka du
ليا
    OUTFLOWS:
duo_secretion = PULSE(10.82,0,.1)
Ξ
    serosal_ill(t) = serosal_ill(t - dt) + (Adsorpt_ill - ile_secretion) * dt
INIT serosal_ill = 0
ħ.
INFLOWS:
    Adsorpt_ill = PULSE(8.83,0,.10)+0*Vol_ileum*ka_il
    OUTFLOWS:
    ile\_secretion = PULSE(1.50,0.1)
    serosal_jej(t) = serosal_jej(t - dt) + (Adsorp_jej - jej_secretion) * dt
    INIT serosal jej = 0
    INFLOWS:
    Adsorp\_jej = PULSE(15.76,0,.1) + 0*Vol\_jej*ka\_je
   OUTFLOWS:
   jej\_secretion = PULSE(2.67,0,.1)
   serosal\_sto(t) = serosal\_sto(t - dt) + (Adsorp\_Stom - Stom\_Secretion) * dt
   INIT serosal sto = 0
   INFLOWS:
   Adsorp_Stom = 0*Vol stom*ka sd
```

```
OUTFLOWS:
     Stom Secretion = PULSE(16.67,0..1)
    Stomach(t) = Stomach(t - dt) + (-SD trans - stom ka) * dt
     INIT Stomach = 1000
    OUTFLOWS:
    SD_trans = if Stomach > 0 then kf_sd*Stomach else 0
    stom_ka = IF Vol_stom*sol_profile >= Stomach THEN Stomach*SA_stom*perm_stom*3600
    ELSE Vol_stom*sol_profile*SA_stom*perm_stom*3600
    total\_drug\_absorbed(t) = total\_drug\_absorbed(t - dt) + (tot\_abs\_rate) * dt
    INIT total drug absorbed = 0
    INFLOWS:
    tot_abs_rate = stom_ka+duo_ka+Jej_ka+Il_ka+colon_ka 5
    Total_Elimination(t) = Total_Elimination(t - dt) + (elimination) * dt
    INIT Total_Elimination = 0
₫
    INFLOWS:
    elimination = amt plasma*k elim
    Vol\_colon(t) = Vol\_colon(t - dt) + (vol\_ij + col\_secretion - vol\_cw - Adsorp\_col) * dt
    INIT Vol colon = 0
UT
Ш
    INFLOWS:
    vol ij = Vol ileum*ka ic
\sqsubseteq col_secretion = 0
<u></u>
OUTFLOWS:
vol_cw = Vol_colon*ka col
Adsorp_col = PULSE(1.67,0,.1)+0*Vol_colon*ka_co
Vol_duod(t) = Vol_duod(t - dt) + (vol_sd + duo_secretion - voil_dj - Adsorp_Duo) * dt
   INIT Vol. duod = 0
   INFLOWS:
   vol sd = kf_sd*Vol_stom
   duo_secretion = PULSE(10.82,0,.1)
   OUTFLOWS:
   voil_dj = Vol duod*ka di
   Adsorp\_Duo = PULSE(10.82,0,.1) + 0*Vol\_duod*ka du
   Vol_ileum(t) = Vol_ileum(t - dt) + (vol_ji + ile_secretion - Adsorpt_ill - vol_ij) * dt
   INIT Vol ileum = 0
   INFLOWS:
   vol_ji = Vol_jej*ka_ji
   ile_secretion = PULSE(1.50,0,.1)
```

```
OUTFLOWS:
    Adsorpt_ill = PULSE(8.83,0,.10)+0*Vol_ileum*ka il
    vol ij = Vol_ileum*ka_ic
    Vol_jej(t) = Vol_jej(t - dt) + (voil_dj + jej_secretion - vol_ji - Adsorp_jej) * dt
    INIT Vol jej = 0
    INFLOWS:
    voil dj = Vol duod*ka di
    jej\_secretion = PULSE(2.67,0,1)
    OUTFLOWS:
    vol_ji = Vol jej*ka ji
    Adsorp_jej = PULSE(15.76,0,1)+0*Vol_jej*ka_je^*
    Vol\_stom(t) = Vol\_stom(t - dt) + (Stom\_Secretion - vol\_sd - Adsorp\_Stom) * dt
    INIT Vol_stom = PULSE(8.33,0,.1)
    INFLOWS:
O
    Stom_Secretion = PULSE(16.67,0,.1)
ū
Ū
    OUTFLOWS:
I
    vol_sd = kf sd*Vol stom
U.
    Adsorp_Stom = 0*Vol stom*ka sd
Ш
    conc_plasma = (amt_plasma/volume)*mg_to_ug
Ш
    k12 = .839
    k21 = .67
<u></u>
    ka co = 1
    ka_{col} = 3
   ka dj = 3
   ka_du = 1
   ka ic = 3
   ka il = 8.83
   ka_j = 1
   ka ii = 3
   ka sd = 1
   kf sd = 2.8
   k elim = .161
   mg_to_ug = 1000
   perm_colon = 3.80e-6
   perm_duo = 1.10e-6
   perm Il = 4.06e-6
   perm_{jej} = 2.17e-6
   perm_stom = 1.10e-6
   ph_s = 1.5
   ph_s_2 = 6.6
   ph_s 3 = 6.6
```

```
ph s 4 = 7.5
         ph_s_5 = 6.6
         SA colon = 138
         SA duo = 125
         SA II = 102
         SA \text{ jej} = 182
         SA stom = 50
        volume = 4*19200
       sol_profile = GRAPH(ph s)
     (1.\overline{00}, 63.0), (1.50, 25.\overline{0}), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3
       3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
       (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
     sol profile 2 = GRAPH(ph_s_2)
     (1.\overline{00}, 63.0), (1.50, 25.0), (2.\overline{00}, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3
     3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
     (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
     sol_profile_3 = GRAPH(ph s 3)
   (1.\overline{00}, 63.0), (1.50, 25.0), (2.\overline{00}, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50,
   3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
   (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
   sol_profile_4 = GRAPH(ph_s 4)
  (1.\overline{00}, 63.0), (1.50, 25.0), (2.\overline{00}, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3
  3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
 (8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
  sol_profile_5 = GRAPH(ph s 5)
 (1.00, 63.0), (1.50, 25.0), (2.00, 10.0), (2.50, 5.00), (3.00, 4.00), (3.50, 3.80), (4.00, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), (4.50, 3.65), 
 3.50), (5.00, 3.65), (5.50, 3.65), (6.00, 3.65), (6.50, 3.65), (7.00, 3.65), (7.50, 3.65), (8.00, 3.65),
(8.50, 4.00), (9.00, 5.00), (9.50, 12.0), (10.0, 23.5)
```

# Appendix 3: Abbreviation Key For GI Model

The legend/key has been divided into sub-sections corresponding to the sub-sections of the model diagram.

Numbered suffixes (1, 2, 3, 4, 5, 6) have been assigned to distinguish between intestinal regions (stomach, duodenum, jejunum, ileum, colon, and waste, respectively).

- l stomach
- 2 duodenum
- 3 jejunum
- 4 ileum
- 5 colon
- 6 waste

For example, VOL 1 is the volume in the stomach, MASS 3 is the insoluble mass in the jejunum. In the equations, COMP 1 indicates the stomach, COMP 2 the duodenum, COMP 3, the jejunum, etc.

Ghosts are listed under the sub-section containing the original reservoir, flow regulator, or converter.

Abbreviations listed in italics are regionally dependent and set up as arrays to allow independent values for each intestinal region.

In general, ADJ as a prefix indicates a calculated parameter value (ADJ = adjusted), while ADJ as a suffix indicates an adjustment parameter (ADJ = adjustment).

#### Intestinal model

#### Reservoirs/Compartments

VOL ABS Fluid volume absorbed

VOL Fluid volume

C REL Mass of drug contained with a formulation or controlled release

device

MASS Insoluble mass of drug (not contained within the formulation or

controlled release device)

SOL Soluble mass of drug

ABSORPTION Mass of drug absorbed

#### Flow regulators

REABS Rate of water absorption VOL OUT Fluid volume transit rate

CR OUT Formulation or controlled release device transit rate

CR INPUT Drug release rate from formulation or controlled release device

MASS OUT Insoluble drug mass transit rate

DISS PRECIP Dissolution rate

SOL OUT Soluble drug mass transit rate

FLUX Absorption rate

# ADJ PARMS (Adjustment Parameters)

VOL ADJ Fluid volume absorption adjustment parameter

DISS ADJ

TRANSIT ADJ

SA ADJ

Dissolution rate adjustment parameter

Transit time adjustment parameter

Surface area adjustment parameter

FLUX ADJ Passive Absorption adjustment parameter
EFFLUX ADJ Efflux or secretion adjustment parameter
CARRIER ADJ Active absorption adjustment parameter

## PARMS (Parameters)

VOL PARM Fluid volume absorption rate constant SURFACE AREA Surface area available for absorption

DOSE The administered dose of drug

INIT VOLUME The administered volume of water or fluid

TIME IN HOURS A clock

pH The physiological pH value

PARACELLULAR A user controlled switch used to adjust absorption based on

absorption mechanism

#### TRANSIT TIME

TRANSFERS GI transit rate constant CUMU TT Cumulative transit time

ADJ TRANSIT TIME Adjusted GI transit time incorporating adjustment parameter and

user input

USER TT INPUT

User controlled adjustments to the GI transit time

## **OUTPUT CALCULATIONS**

ABSORBED TOTAL Total mass of drug absorbed (sum of ABSORPTION 1...5)

ű ₫ Ō ø M Ш Ξ 

FDp% Fraction or the dose absorbed into portal vein x 100

FLUX TOTAL Total absorption rate (sum of FLUX 1...5)

CUM DISS Cumulative drug mass dissolved

CR Release Cumulative drug mass released from formulation

**CUM DISS RATE** Sum of DISS PRECIP 1...5 CR cumrate Summ of CR INPUT 1 5

### PERMEABILITY CALCULATION

**ADJ PERM** Adjusted permeability ncorporating all transport mechanisms and

relevant adjustment parameters

**ACT PE** Active or carrier-mediated absorptive permeability

Km Constant from the Michaelis-Mentin type permeability equation for

active transport

REGIONAL Passive permeability after regional correlation calculation (same as

PASS PE if regional correlation is not used)

PASS PE Passive permeability entered by user

A logical function used in determining the regional correlation RC A logical function used in determining the regional correlation RCSUM

#### SOLUBILITY CALCULATION

USER pH User supplied pH value for which a solubility value is available User supplied solubility value corresponding to the USER pH value **USER SOLUB** ADJ SOLUB Solubility calculated (if necessary) at the appropriate pH value

using the entered USER pH and USER SOLUB values

### CONTROLLED RELEASE CALCULATION

CR RATE The instantaneous release rate from the formulation CR DOSE The total dose contained with the formulation CR AT TIME The cumulative drug mass release profile CR AT LAST The cumulative drug mass release profile

Note: CR AT TIME holds the value at the current time value (t), CR AT LAST holds the value at the immediately preceeding time value (t-1)

#### **CONC CALCULATION**

**CONCENTRATIONS** The dissolved drug concentration

# DISSOLUTION CALCULATION

**PRECIP** Precipitation rate constant DISSOL Dissolution rate constant

ADJ DISS PRECIP Adjusted rate constant incorporating PRECIP, DISSOL and calculated concentration

Appendix 4: Equations, Parameters and Values For GI Model

```
面: ADJ PARMS
            CARRIER_ADJ[COMPS] = 0
            DISS_ADJ[COMP_1] = 1
 5
            DISS_ADJ[COMP 2] = 1
            DISS\_ADJ[COMP\_3] = 1
            DISS\_ADJ[COMP\_4] = 1
            DISS_ADJ[COMP_5] = 1
        EFFLUX_ADJ[COMPS] = 1
FLUX_ADJ[COMP_1] = 1
FLUX_ADJ[COMP_2] = 10
           EFFLUX_ADJ[COMPS] = 1
        FLUX_ADJ[COMP_3] = 8
FLUX_ADJ[COMP_4] = 2
FLUX_ADJ[COMP_5] = 1
10
            SA\_ADJ[COMP\_1] = 1
            SA\_ADJ[COMP\_2] = 1
            SA ADJ[COMP 3] = 1
SA\_ADJ[COMP 4] = 1
ū
           SA\_ADJ[COMP 5] = 1
印
           TRANSIT_ADJ[COMP_1] = 1
O
U
           TRANSIT_ADJ[COMP 2] = 1
Ш
           TRANSIT_ADJ[COMP_3] = 1
Ш
           TRANSIT ADJ[COMP 4] = 1
Ξ
           TRANSIT_ADJ[COMP 5] = 1
<u>_</u>
           VOL_ADJ[COMP_1] = 1
₽
           VOL_ADJ[COMP_2] = 1
N
           VOL_ADJ[COMP 3] = 1
H
           VOL\_ADJ[COMP\_4] = 1
        VOL_ADJ[COMP 5] = 1
        CONC CALCULATION
        ○ CONCENTRATIONS[COMP_1] = if VOL_1=0.0 then 0 else if
           ADJ_SOLUB[COMP_1]<SOL_1/VOL_1 then ADJ_SOLUB[COMP_1] else SOL_1/VOL_1 +
           0*(SOL_2+SOL_5+SOL_3+SOL_4+VOL_3+VOL_2+VOL_4+VOL_5)
        CONCENTRATIONS[COMP_2] = if VOL_2 = 0.0 then 0 else if (VOL_2<1e-6 AND SQL 2<1e-7)
           then 0 else if ADJ_SOLUB[COMP_2]<SOL_2/VOL_2 then ADJ_SOLUB[COMP_2] else
            SOL 2NOL 2
           +0°(SOL_1+SOL_5+SOL_3+SOL_4+VOL_3+VOL_1+VOL_5+VOL_4)
        CONCENTRATIONS[COMP_3] = if VOL_3 = 0.0 then 0 else if (VOL_3<1e-6 AND SQL 3<1e-7)
           then 0 else if ADJ_SOLUB[COMP_3]<SOL_3/VOL_3 then ADJ_SOLUB[COMP_3] else
           SOL 3/VOL 3
           +0*(SOL_1+SOL_2+SOL_4+SOL_5+VOL_5+VOL_4+VOL_1+VOL_2)
        CONCENTRATIONS[COMP_4] = if VOL_4 = 0.0 then 0 else if (VOL_4<1e-6 AND SOL_4<1e-7)
           then 0 else if ADJ_SOLUB[COMP_4]<SOL_4/VOL_4 then ADJ_SOLUB[COMP_4] else
           SOL_4/VOL_4
           +0*(SOL_1+SOL_2+SOL_3+SOL_5+VOL_1+VOL_2+VOL_3+VOL_5)
```

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CONCENTRATIONS[COMP\_5] = if VOL\_5 = 0.0 then 0 else if (VOL\_5<1e-6 AND SOL\_5<1e-7) then 0 else if ADJ\_SOLUB[COMP\_5]<SOL\_5/VOL\_5 then ADJ\_SOLUB[COMP\_5] else SOL 5/VOL 5 +0\*(SOL\_1+SOL\_4+SOL\_3+SOL\_2+VOL\_3+VOL\_1+VOL\_2+VOL\_4) CONTROL RELEASE CALCULATION CR\_DOSE = 0
CR\_RATE = (CR\_AT\_TIME-CR\_AT
CR\_AT\_LAST = GRAPH(TIME-DT) CR\_DOSE = 0 CR\_RATE = (CR\_AT\_TIME-CR\_AT\_LAST)\*20\*(CR\_DOSE/100) (0.00, 0.00), (0.25, 17.7), (0.5, 31.5), (0.75, 42.2), (1.00, 50.6), (1.25, 57.1), (1.50, 62.1), (1.75, 66.1), (2.00, 69.2), (2.25, 71.6), (2.50, 73.4), (2.75, 74.9), (3.00, 76.0), (3.25, 76.9), (3.50, 77.6), (3.75, 78.1), (4.00, 78.5), (4.25, 78.9), (4.50, 79.1), (4.75, 79.3), (5.00, 79.5), (5.25, 79.6), (5.50, 79.6),79.7), (5.75, 79.7), (6.00, 79.8), (6.25, 79.8), (6.50, 79.9), (6.75, 79.9), (7.00, 79.9), (7.25, 79.9), (7.50, 80.0), (7.75, 80.0), (8.00, 80.0), (8.25, 80.0), (8.50, 80.0), (8.75, 80.0), (9.00, 80.0), (9.25, 80.0), (9.50, 80.0), (9.75, 80.0), (10.0, 80.0), (10.3, 80.0), (10.5, 80.0), (10.8, 80.0), (11.0, 80.0), (11.3, 80.0), (11.5, 80.0), (11.8, 80.0), (12.0, 80.0), (12.3, 80.0), (12.5, 80.0), (12.8, 80.0), (13.0, 80.0)... CR\_AT\_TIME = GRAPH(TIME) (0.00, 0.00), (0.25, 17.7), (0.5, 31.5), (0.75, 42.2), (1.00, 50.6), (1.25, 57.1), (1.50, 62.1), (1.75, 66.1), (2.00, 69.2), (2.25, 71.6), (2.50, 73.4), (2.75, 74.9), (3.00, 76.0), (3.25, 76.9), (3.50, 77.6), (3.75, 78.1), (4.00, 78.5), (4.25, 78.9), (4.50, 79.1), (4.75, 79.3), (5.00, 79.5), (5.25, 79.6), (5.50, 79.6),79.7), (5.75, 79.7), (6.00, 79.8), (6.25, 79.8), (6.50, 79.9), (6.75, 79.9), (7.00, 79.9), (7.25, 79.9), (7.50, 80.0), (7.75, 80.0), (8.00, 80.0), (8.25, 80.0), (8.50, 80.0), (8.75, 80.0), (9.00, 80.0), (9.25, 80.0), (9.00, 80.0),80.0), (9.50, 80.0), (9.75, 80.0), (10.0, 80.0), (10.3, 80.0), (10.5, 80.0), (10.8, 80.0), (11.0, 80.0), (11.3, 80.0), (11.5, 80.0), (11.8, 80.0), (12.0, 80.0), (12.3, 80.0), (12.5, 80.0), (12.8, 80.0), (13.0, 80.0)... DISSOLUTION CALCULATION ADJ\_DISS\_PRECIP[COMP\_1] = if VOL\_1=0 then 0 else if (SOL\_1/VOL\_1<ADJ\_SOLUB[COMP\_1]) then (DISSOL[COMP\_1]\*DISS\_ADJ[COMP\_1]\*MASS\_1\*(ADJ\_SOLUB[COMP\_1]-SOL\_1/VOL\_1)) else ((SOL\_1/VOL\_1)-ADJ\_SOLUB[COMP\_1])\*PRECIP[COMP\_1]+ 0\*(MASS\_1+MASS\_2+MASS\_3+MASS\_4+MASS\_5+SOL\_1+SOL\_2+SOL\_3+SOL\_4+SOL\_5+V OL\_1+VOL\_2+VOL\_3+VOL\_4+VOL\_5) ADJ\_DISS\_PRECIP[COMP\_2] = if VOL\_2=0 then 0 else if (SOL\_2/VOL\_2<ADJ\_SOLUB[COMP\_2]) then (DISSOL[COMP\_2]\*DISS\_ADJ[COMP\_2]\*MASS\_2\*(ADJ\_SOLUB[COMP\_2]-SOL\_2/VOL\_2)) else ((SOL\_2/VOL\_2)-ADJ\_SOLUB[COMP\_2])\*PRECIP[COMP\_2] +0\*(MASS\_1+MASS\_2+MASS\_3+MASS\_4+MASS\_5+SOL\_1+SOL\_2+SOL\_3+SOL\_4+SOL\_5+V OL\_1+VOL\_2+VOL\_3+VOL\_4+VOL\_5) ADJ\_DISS\_PRECIP[COMP\_3] = if VOL\_3=0 then 0 else if (SOL\_3/VOL\_3<ADJ\_SOLUB[COMP\_3]) then (DISSOL[COMP\_3]\*DISS\_ADJ[COMP\_3]\*MASS\_3\*(ADJ\_SOLUB[COMP\_3]-SOL\_3/VOL\_3)) else ((SOL\_3/VOL\_3)-ADJ\_SOLUB[COMP\_3])\*PRECIP[COMP\_3] +0\*(MASS\_1+MASS\_2+MASS\_3+MASS\_4+MASS\_5+SOL\_1+SOL\_2+SOL\_3+SOL\_4+SOL\_5+V OL\_1+VOL\_2+VOL\_3+VOL\_4+VOL\_5)

```
ADJ_DISS_PRECIP[COMP_4] = if VOL_4=0 then 0 else if
      (SOL_4/VOL_4<ADJ_SOLUB[COMP_4]) then
      (DISSOL[COMP_4]*DISS_ADJ[COMP_4]*MASS_4*(ADJ_SOLUB[COMP_4]-SOL_4/VOL_4)) else
      ((SOL_4/VOL_4)-ADJ_SOLUB[COMP_4])*PRECIP[COMP_4]
      +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
       OL_1+VOL_2+VOL_3+VOL_4+VOL_5)
   ADJ_DISS_PRECIP[COMP_5] = if VOL_5=0 then 0 else if
      (SOL_5/VOL_5<ADJ_SOLUB[COMP_5]) then
      (DISSOL[COMP_5]*DISS_ADJ[COMP_5]*MASS_5*(ADJ_SOLUB[COMP_5]-SOL_5/VOL_5)) else
      ((SOL_5/VOL_5)-ADJ_SOLUB[COMP_5])*PRECIP[COMP_5]
      +0*(MASS_1+MASS_2+MASS_3+MASS_4+MASS_5+SOL_1+SOL_2+SOL_3+SOL_4+SOL_5+V
   DISSOL[COMP_1] = 1
      OL_1+VOL_2+VOL_3+VOL_4+VOL_5)
      DISSOL[COMP_3] = 1
      DISSOL[COMP_4] = 1
     DISSOL[COMP_5] = 1
      PRECIP[COMP_1] = 10
9
      PRECIP[COMP_2] = 10
      PRECIP[COMP_3] = 10
      PRECIP[COMP 4] = 10
Ų
      PRECIP[COMP_5] = 10
   INPUTS
   INTESTINAL MODEL
  ABSORPTION_1(t) = ABSORPTION_1(t - dt) + (FLUX_1) * dt
      INIT ABSORPTION_1 = 0
ä
      INFLOWS:
TLI

→ FLUX_1 =
CONCENTRATIONS[COMP_1]*ADJ_PERM[COMP_1]*SURFACE_AREA[COMP_1]
ABSORPTION_2(t) = ABSORPTION_2(t - dt) + (FLUX_2) * dt
      INIT ABSORPTION 2 = 0
      INFLOWS:

☆ FLUX_2 = 
            CONCENTRATIONS[COMP_2]*ADJ_PERM[COMP_2]*SURFACE_AREA[COMP_2]
  ABSORPTION_3(t) = ABSORPTION_3(t - dt) + (FLUX_3) * dt
      INIT ABSORPTION 3 = 0
      INFLOWS:

⇒ FLUX_3 =
           CONCENTRATIONS[COMP_3]*ADJ_PERM[COMP_3]*SURFACE_AREA[COMP_3]
  ABSORPTION_4(t) = ABSORPTION_4(t - dt) + (FLUX_4) * dt
      INIT ABSORPTION_4 = 0
      INFLOWS:
```

```
☆ FLUX_4 =
             CONCENTRATIONS[COMP_4]*ADJ_PERM[COMP_4]*SURFACE_AREA[COMP_4]
   ABSORPTION_5(t) = ABSORPTION_5(t - dt) + (FLUX 5) * dt
       INIT ABSORPTION_5 = 0
       INFLOWS:

⇒ FLUX_5 = if time<32 then
</p>
            CONCENTRATIONS[COMP_5]*ADJ_PERM[COMP_5]*SURFACE_AREA[COMP_5]*(32-ti
             me)/48*(VOL 5/17.2) else 0
   C_REL_1(t) = C_REL_1(t - dt) + (- CR_OUT_1 - CR_INPUT_1) * dt
       INIT C_REL_1 = CR_DOSE
       OUTFLOWS:
         ⇔ CR_OUT_1 = IF TIME >= CUMU_TT[COMP_1] THEN C_REL_1*10000 ELSE 0
         CR_INPUT_1 = if TIME>CUMU_TT[COMP_1] then 0 else CR_RATE
     C_REL_2(t) = C_REL_2(t - dt) + (CR_OUT_1 - CR_OUT_2 - CR_INPUT_2) * dt
      INIT C REL 2 = 0
       INFLOWS:
         증 CR_OUT_1 = IF TIME >= CUMU_TT[COMP_1] THEN C_REL_1*10000 ELSE 0
ū
       OUTFLOWS:
⇔ CR_OUT_2 = IF TIME >= CUMU_TT[COMP_2] THEN C_REL_2*10000 ELSE 0
Ö
         ⇔ CR_INPUT_2 = if TIME>CUMU_TT[COMP_2] then 0 else CR_RATE
₽
C_REL_3(t) = C_REL_3(t - dt) + (CR_OUT_2 - CR_OUT_3 - CR_INPUT_3) * dt
      INIT C REL 3 = 0
Ш
       INFLOWS:
Ш
         CR_OUT_2 = IF TIME >= CUMU_TT[COMP_2] THEN C_REL_2*10000 ELSE 0
OUTFLOWS:
#

☆ CR_OUT_3 = IF TIME >= CUMU_TT[COMP_3] THEN C_REL_3*10000 ELSE 0

N
         CR_INPUT_3 = if TIME > CUMU_TT[COMP_3] then 0 else CR_RATE
  C_REL_4(t) = C_REL_4(t - dt) + (CR_OUT_3 - CR_OUT_4 - CR_INPUT_4) * dt
      INIT C_REL_4 = 0
       INFLOWS:
        CR_OUT_3 = IF TIME >= CUMU_TT[COMP_3] THEN C_REL_3*10000 ELSE 0
       OUTFLOWS:
        ☆ CR_OUT_4 = IF TIME >= CUMU_TT[COMP_4] THEN C_REL_4*10000 ELSE 0

→ CR_INPUT_4 = if TIME>CUMU_TT[COMP_4] then 0 else CR_RATE

  C_REL_5(t) = C_REL_5(t - dt) + (CR_OUT_4 - CR_OUT_5 - CR_INPUT_5) * dt
      INIT C_REL_5 = 0
       INFLOWS:
        CR_OUT_4 = IF TIME >= CUMU_TT[COMP_4] THEN C_REL_4*10000 ELSE 0
       OUTFLOWS:
        CR_OUT_5 = IF TIME >= CUMU_TT[COMP_5] THEN C_REL_5*10000 ELSE 0
        ☆ CR_INPUT_5 = if TIME>CUMU_TT[COMP_5] then 0 else CR_RATE
  \square C_REL_6(t) = C_REL_6(t - dt) + (CR_OUT_5) * dt
      INIT C REL 6 = 0
      INFLOWS:

★ CR_OUT_5 = IF TIME >= CUMU_TT[COMP_5] THEN C_REL_5*10000 ELSE 0
```

```
MASS_1(t) = MASS_1(t - dt) + (CR_INPUT_1 - MASS_OUT_1 - DISS_PRECIP_1) * dt
    INIT MASS_1 = DOSE
    INFLOWS:
      ☆ CR_INPUT_1 = if TIME>CUMU_TT[COMP_1] then 0 else CR_RATE
     OUTFLOWS:

★ MASS_OUT_1 = MASS_1*TRANSFERS[COMP_1]

⇒ DISS_PRECIP_1 = ADJ_DISS_PRECIP[COMP_1]

MASS_2(t) = MASS_2(t - dt) + (MASS_OUT_1 + CR_INPUT_2 - MASS_OUT_2 -
    DISS_PRECIP_2) * dt
    INIT MASS 2 = 0
    INFLOWS:
      ★ MASS_OUT_1 = MASS_1*TRANSFERS[COMP 1]

★ CR_INPUT_2 = if TIME>CUMU_TT[COMP_2] then 0 else CR_RATE

    OUTFLOWS:
      MASS_OUT_2 = MASS_2*TRANSFERS[COMP 2]

⇒ DISS_PRECIP_2 = ADJ_DISS_PRECIP[COMP_2]

MASS_3(t) = MASS_3(t - dt) + (CR_INPUT_3 + MASS_OUT_2 - MASS_OUT_3 -
    DISS_PRECIP_3) * dt
    INIT MASS_3 = 0
    INFLOWS:
      CR_INPUT_3 = if TIME > CUMU_TT[COMP_3] then 0 else CR_RATE
      ★ MASS_OUT_2 = MASS_2*TRANSFERS[COMP 2]
    OUTFLOWS:

☆ MASS_OUT_3 = MASS_3*TRANSFERS[COMP 3]

      ⇒ DISS_PRECIP_3 = ADJ_DISS_PRECIP[COMP 3]
MASS_4(t) = MASS_4(t - dt) + (CR_INPUT_4 + MASS_OUT_3 - MASS_OUT_4 -
   DISS_PRECIP_4) * dt
   INIT MASS_4 = 0
    INFLOWS:
      ★ CR_INPUT_4 = if TIME>CUMU_TT[COMP_4] then 0 else CR_RATE
      * MASS_OUT_3 = MASS_3*TRANSFERS(COMP 3)
    OUTFLOWS:
      MASS_OUT_4 = MASS_4*TRANSFERS[COMP_4]

⇒ DISS_PRECIP_4 = ADJ_DISS_PRECIP[COMP_4]

MASS_5(t) = MASS_5(t - dt) + (CR_INPUT_5 + MASS_OUT_4 - MASS_OUT_5 -
   DISS PRECIP 5) * dt
   INIT MASS_5 = 0
    INFLOWS:
      ☆ CR_INPUT_5 = if TIME>CUMU_TT[COMP_5] then 0 else CR_RATE

☆ MASS_OUT_4 = MASS_4*TRANSFERS[COMP_4]

    OUTFLOWS:
      ☆ MASS_OUT_5 = if time>4 then MASS_5*TRANSFERS[COMP_5] else 0

⇒ DISS_PRECIP_5 = ADJ_DISS_PRECIP[COMP_5]

\square MASS_6(t) = MASS_6(t - dt) + (MASS_OUT_5) * dt
   INIT MASS_6 = 0
    INFLOWS:
```

```
★ MASS_OUT_5 = if tim >4 th n MASS_5*TRANSFERS[COMP_5] else 0
   SOL_1(t) = SOL_1(t - dt) + (DISS_PRECIP_1 - SOL_OUT_1 - FLUX_1) * dt
       INIT SOL_1 = 0
        INFLOWS:

⇒ DISS_PRECIP_1 = ADJ_DISS_PRECIP[COMP_1]

        OUTFLOWS:

⇒ SOL_OUT_1 = SOL_1*TRANSFERS[COMP 1]

⇒ FLUX_1 =
             CONCENTRATIONS[COMP_1]*ADJ_PERM[COMP_1]*SURFACE_AREA[COMP_1]
   \square SOL_2(t) = SOL_2(t - dt) + (SOL_OUT_1 + DISS_PRECIP_2 - SOL_OUT_2 - FLUX_2) * dt
       INIT SOL 2 = 0
        INFLOWS:

⇒ SOL_OUT_1 = SOL_1*TRANSFERS[COMP_1]

         ㅎ DISS_PRECIP_2 = ADJ_DISS_PRECIP[COMP 2]
        OUTFLOWS:

⇒ SOL_OUT_2 = SOL_2*TRANSFERS[COMP_2]

→ FLUX 2 = 
₫
            CONCENTRATIONS[COMP_2]*ADJ_PERM[COMP_2]*SURFACE_AREA[COMP_2]
m
Ū
      SOL_3(t) = SOL_3(t - dt) + (DISS_PRECIP_3 + SOL_OUT_2 - SOL_OUT_3 - FLUX_3) * dt
Ų
       INIT SOL 3 = 0
Ш
Ш
       INFLOWS:
≘
         DISS_PRECIP_3 = ADJ_DISS_PRECIP[COMP 3]
<u>ļ</u>

☆ SOL_OUT_2 = SOL_2*TRANSFERS[COMP 2]

OUTFLOWS:
N
         SOL_OUT_3 = SOL_3*TRANSFERS[COMP 3]
<u>ئىڭ</u>

⇒ FLUX_3 = 
酉
            CONCENTRATIONS[COMP_3]*ADJ_PERM[COMP_3]*SURFACE_AREA[COMP_3]
Ŀ
  \square SOL_4(t) = SOL_4(t - dt) + (DISS_PRECIP_4 + SOL_OUT_3 - SOL_OUT_4 - FLUX_4) + dt
      INIT SOL_4 = 0
       INFLOWS:

⇒ DISS_PRECIP_4 = ADJ_DISS_PRECIP[COMP_4]

⇒ SOL_OUT_3 = SOL_3*TRANSFERS(COMP 3)

       OUTFLOWS:

⇒ SOL_OUT_4 = SOL_4*TRANSFERS[COMP_4]

→ FLUX 4 = 
            CONCENTRATIONS[COMP_4]*ADJ_PERM[COMP_4]*SURFACE_AREA[COMP_4]
  SOL_5(t) = SOL_5(t - dt) + (DISS_PRECIP_5 + SOL_OUT_4 - SOL_OUT_5 - FLUX_5) • dt
      INIT SOL 5 = 0
       INFLOWS:
```

```
⇒ DISS_PRECIP_5 = ADJ_DISS_PRECIP[COMP 5]

⇒ SOL_OUT_4 = SOL_4°TRANSFERS[COMP 4]

      OUTFLOWS:
        ⇒ SOL_OUT_5 = if time>4 then SOL_5*TRANSFERS[COMP_5] else 0

⇔ FLUX_5 = if time<32 then
</p>
           CONCENTRATIONS[COMP_5]*ADJ_PERM[COMP_5]*SURFACE_AREA[COMP_5]*(32-ti
           me)/48*(VOL_5/17.2) else 0
  \subseteq SOL_6(t) = SOL_6(t - dt) + (SOL_OUT_5) * dt
     INIT SOL 6 = 0
      INFLOWS:

☆ SOL_OUT_5 = if time>4 then SOL_5*TRANSFERS[COMP_5] else 0

  INIT VOL_1 = INIT_VOLUME
      OUTFLOWS:

⇒ REABS_1 = VOL_1*VOL_PARM[COMP_1]

        \Box VOL_2(t) = VOL_2(t - dt) + (VOL_OUT_1 - VOL_OUT_2 - REABS 2) * dt
     INIT VOL 2 = 0
ū
      INFLOWS:
₽

☆ VOL_OUT_1 = VOL_1*TRANSFERS[COMP_1]

M
      OUTFLOWS:
ū

      ★ VOL_OUT_2 = VOL_2*TRANSFERS[COMP 2]

U
       REABS_2 = VOL_2*VOL_PARM[COMP_2]
UOL_3(t) = VOL_3(t - dt) + (VOL_OUT_2 - VOL_OUT_3 - REABS 3) * dt
     INIT VOL 3 = 0
Ξ
      INFLOWS:
ļ.

        ★ VOL_OUT_2 = VOL_2*TRANSFERS[COMP 2]

<u>!-:</u>
N
      OUTFLOWS:

★ VOL_OUT_3 = VOL_3*TRANSFERS[COMP_3]

       * REABS_3 = VOL_3*VOL_PARM[COMP_3]
INIT VOL 4 = 0
     INFLOWS:

⇒ VOL_OUT_3 = VOL_3*TRANSFERS[COMP_3]

      OUTFLOWS:

☆ VOL_OUT_4 = VOL_4*TRANSFERS[COMP 4]
       REABS_4 = VOL_4*VOL_PARM[COMP 4]
  VOL_5(t) = VOL_5(t - dt) + (VOL_OUT_4 - VOL_OUT_5 - REABS_5) * dt
     INIT VOL 5=0
     INFLOWS:

★ VOL_OUT_4 = VOL_4*TRANSFERS[COMP_4]
     OUTFLOWS:

    Ö VOL_OUT_5 = VOL_5*TRANSFERS[COMP 5]
       REABS_5 = VOL_5*VOL_PARM[COMP_5]
 \bigvee VOL_6(t) = VOL_6(t - dt) + (VOL_OUT_5) * dt
    INIT VOL 6 = 0
```

```
INFLOWS:
          ㅎ VOL_OUT_5 = VOL_5 TRANSFERS[COMP_5]
      VOL_ABS_1(t) = VOL_ABS_1(t - dt) + (REABS_1) * dt
        INIT VOL_ABS 1 = 0
        INFLOWS:
          REABS_1 = VOL_1*VOL_PARM[COMP_1]
    \bigvee VOL_ABS_2(t) = VOL_ABS_2(t - dt) + (REABS_2) • dt
        INIT VOL ABS 2 = 0
        INFLOWS:
          REABS_2 = VOL_2*VOL_PARM[COMP 2]
    \bigcirc VOL_ABS_3(t) = VOL_ABS_3(t - dt) + (REABS_3) * dt
       INIT VOL_ABS_3 = 0
        INFLOWS:
          REABS_3 = VOL_3*VOL_PARM[COMP 3]
    INIT VOL ABS 4 = 0
        INFLOWS:

★ REABS_4 = VOL_4*VOL_PARM[COMP_4]

o
   VOL_ABS_5(t) = VOL_ABS_5(t - dt) + (REABS_5) * dt
o
       INIT VOL ABS 5 = 0
Ø
        INFLOWS:
Ū
         REABS_5 = VOL_5*VOL_PARM[COMP 5]
U
    MULTI DOSE CALCULATION
   OUTPUT CALCULATIONS
   CR_Release(t) = CR_Release(t - dt) + (CR_cumrate) * dt
Ξ
      . INIT CR_Release = 0
#
INFLOWS:
ΠJ
         CR_cumrate = CR_INPUT_1+CR_INPUT_2+CR_INPUT_3+CR_INPUT_4+CR_INPUT_5
CUM_DISS(t) = CUM_DISS(t - dt) + (CUMM_DISS_RATE) * dt
       INIT CUM_DISS = 0
       INFLOWS:

☆ CUMM_DISS_RATE = 
            DISS_PRECIP_1+DISS_PRECIP_2+DISS_PRECIP_3+DISS_PRECIP_4+DISS_PRECIP
   ABSORBED_TOTAL = ABSORPTION_2+ABSORPTION_3+ABSORPTION_4+ABSORPTION_5
      FDp% = ABSORBED_TOTAL/DOSE*100
   FLUX_TOTAL = FLUX_2+FLUX_3+FLUX_4+FLUX_5
PARMS
   O DOSE = 1000
   ○ INIT_VOLUME = 100
○ PARACELLULAR = 1
      pH[COMP_1] = 1.5
      pH[COMP 2] = 5
      pH[COMP_3] = 6.5
```

```
pH[COMP_4] = 7
       pH[COMP_5] = 6.5
    SURFACE_AREA[COMP_1] = if PARACELLULAR =0 then 50*SA_ADJ[COMP_1] else
       50*SA ADJ[COMP 1]
    SURFACE_AREA[COMP_2] = if PARACELLULAR=0 then 150*SA_ADJ[COMP_2] else
       7.5*SA_ADJ[COMP_2]
    SURFACE_AREA[COMP_3] = if PARACELLULAR=0 then 1000*SA_ADJ[COMP_3] else
       50"SA_ADJ[COMP 3]
    SURFACE_AREA[COMP_4] = if PARACELLULAR=0 then 1000*SA_ADJ[COMP_4] else
       50°SA_ADJ[COMP_4]
    SURFACE_AREA[COMP_5] = if PARACELLULAR=0 then 850*SA_ADJ[COMP_5] else
       42.5*SA_ADJ[COMP_5]
   TIME_IN_HOURS = TIME
     VOL_PARM[COMP_1] = 0*VOL_ADJ[COMP_1]
      VOL_PARM[COMP_2] = 0*VOL_ADJ[COMP_2]
O VOL_PARM[COMP_3] = 1.75*VOL_ADJ[COMP_3]
      VOL_PARM[COMP_4] = 1.75*VOL_ADJ[COMP_4]
     VOL_PARM[COMP_5] = 0.10*VOL_ADJ[COMP_5]
   PERMEABILITY CALCULATION
    ACT_PE[COMPS] = [0.
U
      0,
Ш
       0,
لِيَا
      0,
≅
      0]
   ADJ_PERM[COMP 1] =
      (2/(1+EFFLUX_ADJ[COMP_1]))*REGIONAL[COMP_1]*FLUX_ADJ[COMP_1]*3600+(CARRIER_
N
      DJ[COMP_1]*ACT_PE[COMP_1]*3600/(1+(CONCENTRATIONS[COMP_1]/(Km[COMP_1]))))*0
H
   ADJ_PERM[COMP_2] =
      (2/(1+EFFLUX_ADJ[COMP_2]))*REGIONAL[COMP_2]*FLUX_ADJ[COMP_2]*3600+(CARRIER_
      DJ[COMP_2]*ACT_PE[COMP_2]*3600/(1+(CONCENTRATIONS[COMP_2]/(Km[COMP_2]))))
   ADJ_PERM[COMP 3] =
      (2/(1+EFFLUX_ADJ[COMP_3]))*REGIONAL[COMP_3]*FLUX_ADJ[COMP_3]*3600+(CARRIER_
      DJ[COMP_3]*ACT_PE[COMP_3]*3600/(1+(CONCENTRATIONS[COMP_3]/(Km[COMP_3]))))
  ADJ_PERM[COMP_4] =
      (2/(1+EFFLUX_ADJ[COMP_4]))*REGIONAL[COMP_4]*FLUX_ADJ[COMP_4]*3600+(CARRIER_
      DJ[COMP_4]*ACT_PE[COMP_4]*3600/(1+(CONCENTRATIONS[COMP_4]/(Km[COMP_4]))))
  ADJ_PERM[COMP_5] =
     (2/(1+EFFLUX_ADJ[COMP_5]))*REGIONAL[COMP_5]*FLUX_ADJ[COMP_5]*3600+(CARRIER_
     DJ[COMP_5]*ACT_PE[COMP_5]*3600/(1+(CONCENTRATIONS[COMP_5]/(Km[COMP_5]))))
```

```
    Km[COMPS] = [1]

       1,
       1,
   PASS_PE[COMPS] = [0
       1.10E-06
       2.17E-06.
       4.06E-06.
       3.80E-06]
   RC[COMP_1] = PASS_PE[COMP_1]*0
     RC[COMP_2] = IF PASS_PE[COMP_2]>0 THEN 1 ELSE 0
      RC[COMP_3] = IF PASS_PE[COMP_3]>0 THEN 2 ELSE 0
      RC[COMP_4] = IF PASS_PE[COMP_4]>0 THEN 4 ELSE 0
      RC[COMP_5] = PASS_PE[COMP_5]*0
  RCSUM = RC[COMP_2]+RC[COMP_3]+RC[COMP_4]
   REGIONAL[COMP_1] = PASS_PE[COMP_1]+RCSUM*0
J
      REGIONAL[COMP_2] = if RCSUM=2 then
      (EXP( -9.011926 + 2.594378 *LOGN(1/PASS_PE[COMP_2]) -0.065515
Ī
      *LOGN(1/PASS_PE[COMP_2])^2))^(-1) else
Ō
      if RCSUM=4 then
Lī
Ш
      (EXP(-0.369414*LOGN(1/PASS_PE[COMP_4])+0.23756*LOGN(1/PASS_PE[COMP_4])^2-0.009
Ш
      9719*LOGN(1/PASS_PE[COMP_4])^3))^(-1) else
      if RCSUM=6 then
      0.5°(EXP( -9.011926 + 2.594378 *LOGN(1/PASS_PE[COMP_3]) -0.065515
T.
      *LOGN(1/PASS_PE[COMP_3])^2))^(-1)
      +0.5*(EXP( -21.009845 + 4.544238 *LOGN(1/PASS_PE[COMP_4]) -0.140815
!!!
*LOGN(1/PASS_PE[COMP_4])^2))^(-1) else
      PASS_PE[COMP_2]
  (EXP(-3.238469 + 1.509131 *LOGN(1/PASS_PE[COMP_2]) -0.022109
     *LOGN(1/PASS_PE[COMP_2])^(-1) else
     if RCSUM=4 then
     (EXP(-0.093739*LOGN(1/PASS_PE[COMP_4])+0.182344*LOGN(1/PASS_PE[COMP_4])^2-0.00
     23631*LOGN(1/PASS_PE[COMP_4])^3))^(-1) else
     if RCSUM=5 then
     0.5*(EXP( -3.238469 + 1.509131 *LOGN(1/PASS_PE[COMP_2]) -0.022109
     *LOGN(1/PASS_PE[COMP_2])^2))^(-1)
     +0.5°(EXP( -15.415683 + 3.543563 *LOGN(1/PASS_PE[COMP_4]) -0.100318
     *LOGN(1/PASS_PE[COMP_4])^2))^(-1) else
     PASS_PE[COMP_3]
```

```
REGIONAL[COMP_4] = if RCSUM=1 then
       (EXP( 14.455255 -1.264630 *LOGN(1/PASS_PE[COMP_2]) + 0.082015
       *LOGN(1/PASS_PE[COMP_2])^2))^(-1) else
       if RCSUM=2 then
       (EXP( 11.480333 -0.791109 *LOGN(1/PASS_PE[COMP_3]) + 0.066063
       *LOGN(1/PASS_PE[COMP_3])^2))^(-1) else
       if RCSUM=3 then
       0.5*(EXP( 14.455255 -1.264630 *LOGN(1/PASS_PE[COMP_2]) + 0.082015
       *LOGN(1/PASS_PE[COMP_2])^2))^(-1)
       +0.5*(EXP( 11.480333 -0.791109 *LOGN(1/PASS_PE[COMP_3]) + 0.066063
       *LOGN(1/PASS_PE[COMP_3])^2))^(-1) else
       PASS_PE[COMP_4]
    REGIONAL[COMP_5] = PASS_PE[COMP_5] +RCSUM*0
SOLUBILIY CALCULATION
   C ADJ_SOLUB[COMP_1] = if USER_pH[COMP_1]>=pH[COMP_1] then USER_SOLUB[COMP_1]
       else
       ((USER_SOLUB[COMP_2]-USER_SOLUB[COMP_1])/(USER_pH[COMP_2]-USER_pH[COMP_1]
))*(pH[COMP_1]-USER_pH[COMP_1])+USER_SOLUB[COMP_1]
   ADJ_SOLUB[COMP_2] = if USER_pH[COMP_2]=pH[COMP_2] then USER_SOLUB[COMP_2]
4
Ö
      else if USER_pH[COMP_2]<pH[COMP_2] then
      ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
Ō
      ))*(pH[COMP_2]-USER_pH[COMP_2])+USER_SOLUB[COMP_2] else
Ш
      ((USER_SOLUB[COMP_2]-USER_SOLUB[COMP_1])/(USER_pH[COMP_2]-USER_pH[COMP_1]
Ш
      ))*(pH[COMP_2]-USER_pH[COMP_1])+USER_SOLUB[COMP_1]
Ш
      ADJ_SOLUB[COMP_3] = if USER_pH[COMP_3]=pH[COMP_3] then USER_SOLUB[COMP_3]
      else if USER_pH[COMP_3]<pH[COMP_3] then
      ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
<u>_</u>
      ))*(pH[COMP_3]-USER_pH[COMP_3])+USER_SOLUB[COMP_3] else
N
      ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
井
      ))*(pH[COMP_3]-USER_pH[COMP_2])+USER_SOLUB[COMP_2]
ADJ_SOLUB[COMP_4] = if USER_pH[COMP_4]=pH[COMP_4] then USER_SOLUB[COMP_4]
      else if USER_pH[COMP_4]<pH[COMP_4] then
      ((USER_SOLUB[COMP_5]-USER_SOLUB[COMP_4])/(USER_pH[COMP_5]-USER_pH[COMP_4]
      ))*(pH[COMP_4]-USER_pH[COMP_4])+USER_SOLUB[COMP_4] else
      ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
      ))*(pH[COMP_4]-USER_pH[COMP_3])+USER_SOLUB[COMP_3]
  ADJ_SOLUB[COMP_5] = if USER_pH[COMP_3]=pH[COMP_3] then USER_SOLUB[COMP_3]
      else if USER_pH[COMP_3]<pH[COMP_3] then
      ((USER_SOLUB[COMP_4]-USER_SOLUB[COMP_3])/(USER_pH[COMP_4]-USER_pH[COMP_3]
      ))*(pH[COMP_3]-USER_pH[COMP_3])+USER_SOLUB[COMP_3] else
      ((USER_SOLUB[COMP_3]-USER_SOLUB[COMP_2])/(USER_pH[COMP_3]-USER_pH[COMP_2]
      ))*(pH[COMP_3]-USER_pH[COMP_2])+USER_SOLUB[COMP_2]
  USER_pH[COMPS] = [1.5]
     5,
     6.5.
     7,
     7.5
```

```
USER_SOLUB[COMPS] = [31.
       3.65 .
      3.65.
      3.65.
      3.651
   TRANSIT TIME
      ADJ_TRANSIT_TIME[COMP_1] = .5*TRANSIT_ADJ[COMP_1]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_2] = .25*TRANSIT_ADJ[COMP_2]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_3] = 1.5*TRANSIT_ADJ[COMP_3]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_4] = 1.5*TRANSIT_ADJ[COMP_4]*USER_TT_INPUT
      ADJ_TRANSIT_TIME[COMP_5] = 24*TRANSIT_ADJ[COMP_5]*USER_TT_INPUT
      CUMU_TT[COMP_1] = ADJ_TRANSIT_TIME[COMP_1]
      CUMU_TT[COMP_2] = ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]
CUMU_TT[COMP_3] =
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
3]
   CUMU_TT[COMP_4] =
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
П
      3]+ADJ_TRANSIT_TIME[COMP_4]
   CUMU_TT[COMP_5] =
Ш
      ADJ_TRANSIT_TIME[COMP_1]+ADJ_TRANSIT_TIME[COMP_2]+ADJ_TRANSIT_TIME[COMP_
      3]+ADJ_TRANSIT_TIME[COMP_4]+ADJ_TRANSIT_TIME[COMP_5]
      TRANSFERS[COMP_1] = LOGN(10)ADJ_TRANSIT_TIME[COMP_1]
TRANSFERS[COMP_2] = LOGN(10)ADJ_TRANSIT_TIME[COMP_2]
      TRANSFERS[COMP_3] = LOGN(10)ADJ_TRANSIT_TIME[COMP_3]
      TRANSFERS[COMP_4] = LOGN(10)ADJ_TRANSIT_TIME[COMP_4]
      TRANSFERS[COMP_5] = LOGN(10)ADJ_TRANSIT_TIME[COMP_5]
      USER_TT_INPUT = 1
```